

New Quenching and Deformation Dilatometer at FRM II

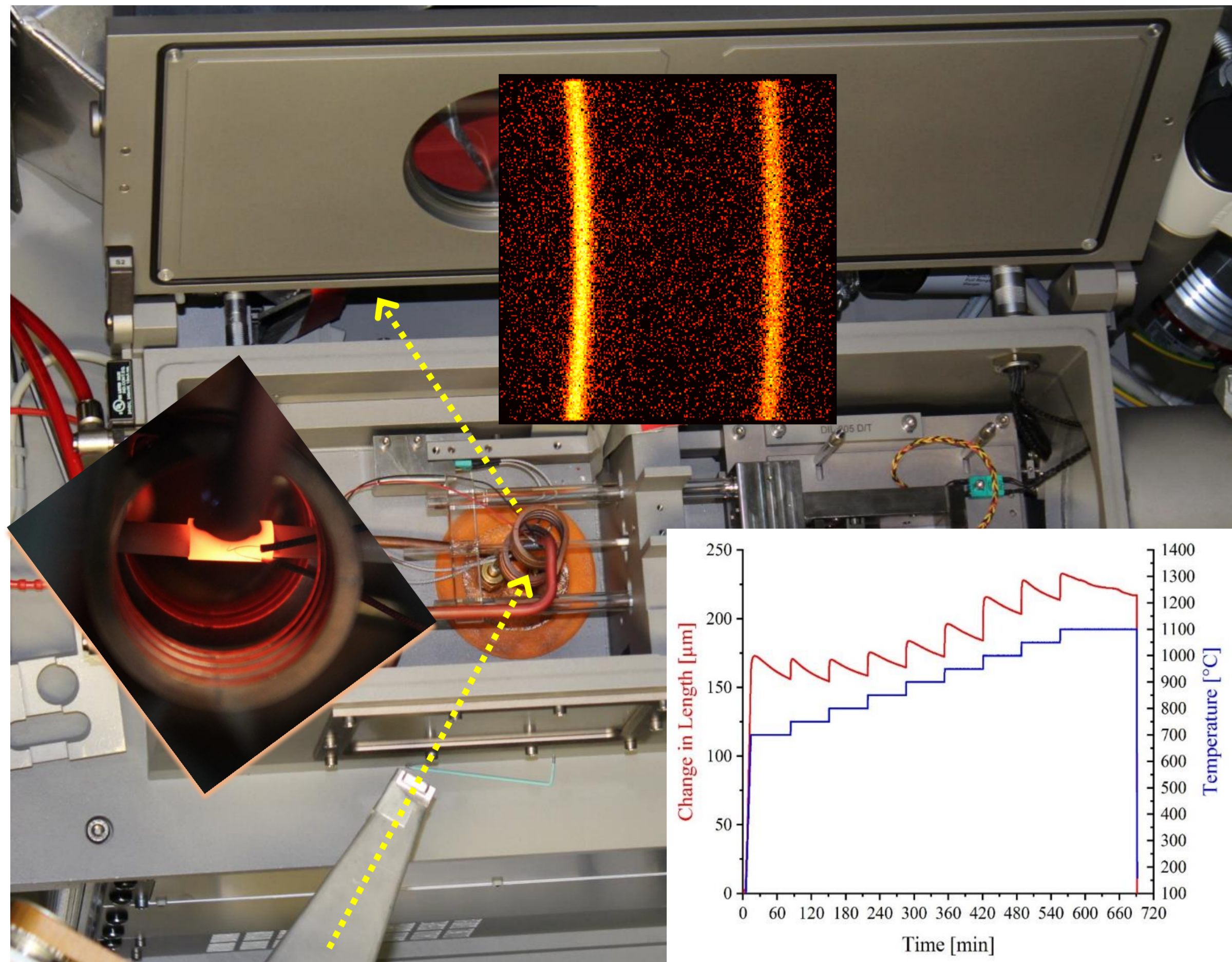
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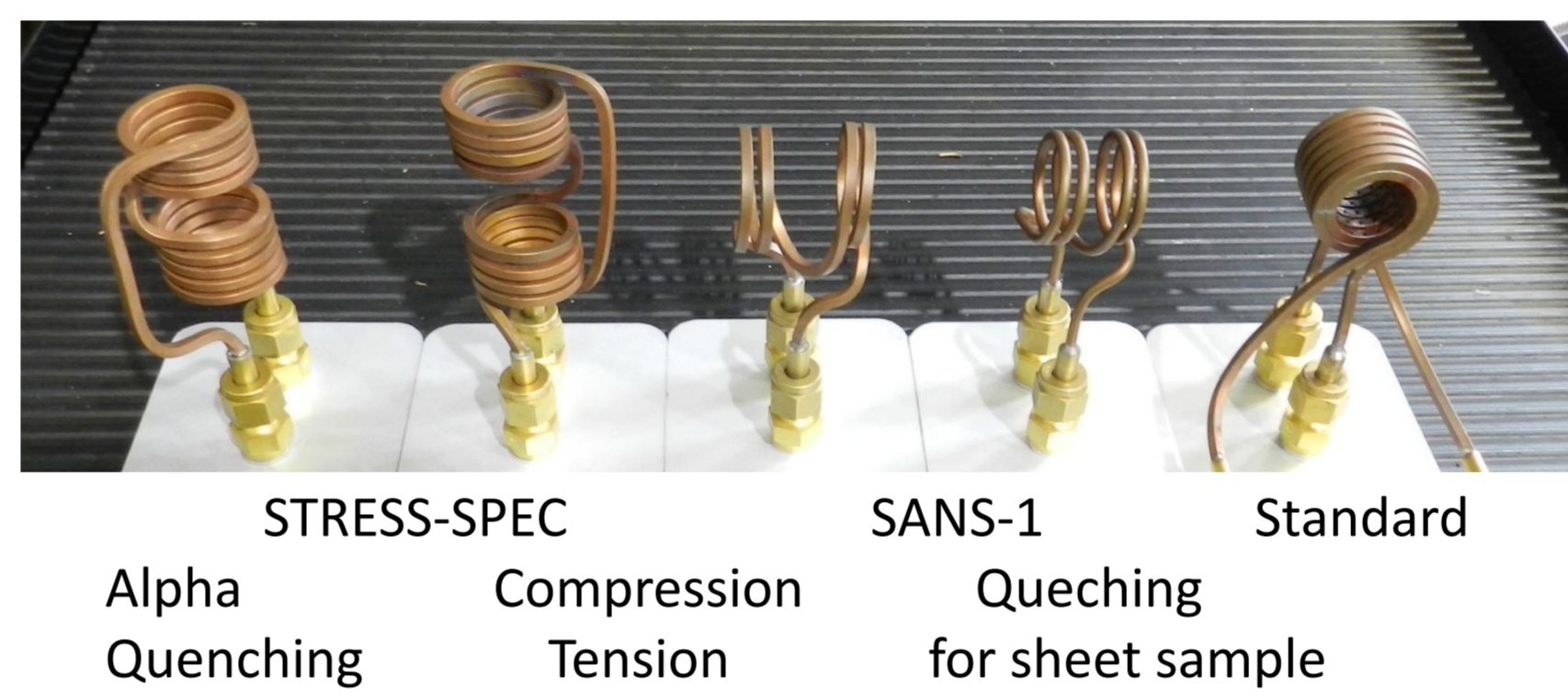
Combination of dilatometer DIL 805A/D/T with neutron diffraction at FRM II (STRESS-SPEC)



Neutron beam path and experimental signal during the in-situ measurement



Technical details



Different types of heating coils

	Alpha mode	Compression mode	Tension mode
Temperature Range	50°C to 1500°C With special designed heating coil up to 1450°C at STRESS-SPEC and 1100°C at SANS-1		
T. Resolution	0.05 °C		
Heating rate	4000 °C/s	100 °C/s	100 °C/s
Cooling rate	2500 °C/s	100 °C/s	100 °C/s
Length change	10 nm	50 nm	50 nm
Deformation force		Up to 20 kN	Up to 8 kN
Deformation rate		0.01 – 200 mm/s	0.01 – 20 mm/s
Strain rate		0.001 – 20 s ⁻¹	0.001 – 20 s ⁻¹
Min. Gauge length		3 mm	3 mm

Publication:

X. H. Li, M. Hofmann, M. Landesberger, M. Reiberg, X. Zhang, E. Werner, W. M. Gan.: A unique quenching and deformation dilatometer for combined in situ neutron diffraction analysis of engineering materials; *Adv. Eng. Mater.* (2021) 2100163; DOI: 10.1002/adem.202100163

Recent Examples

High-temperature Phase Characterization in AlCrFeNiTi alloys

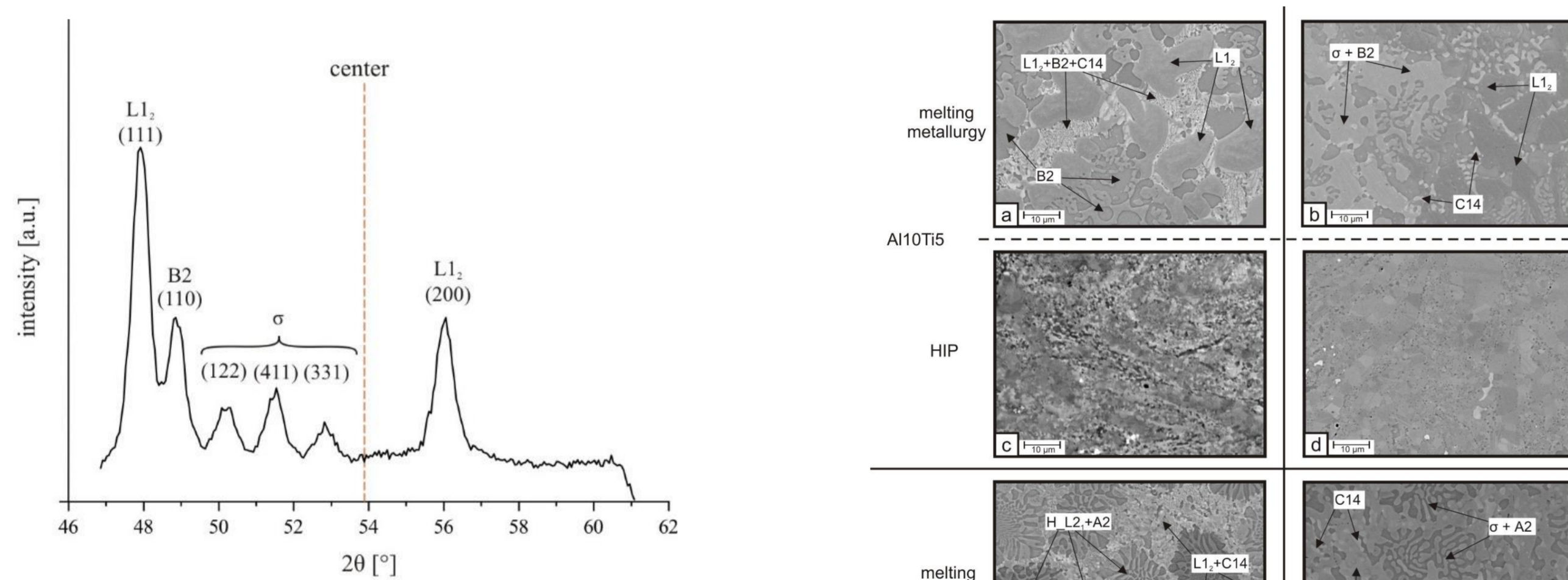


Fig.1 Neutron-diffractogram of composition Al10Ti10 as-HIP at 900 °C. Tagged peaks are used for determination of phase-amounts of L₁₂, B2 and σ.

$$I_{(hkl)\alpha} = \frac{C |B(hkl)\alpha|^2 V_\alpha}{\mu_s}$$

C is a constant related to an experimental setup and remains the same in a single experiment, B(hkl)α is the structure factor of reflection (hkl) of phase α, V_α is the volume fraction of phase α and μ_s is the mass absorption coefficient of the specimen.

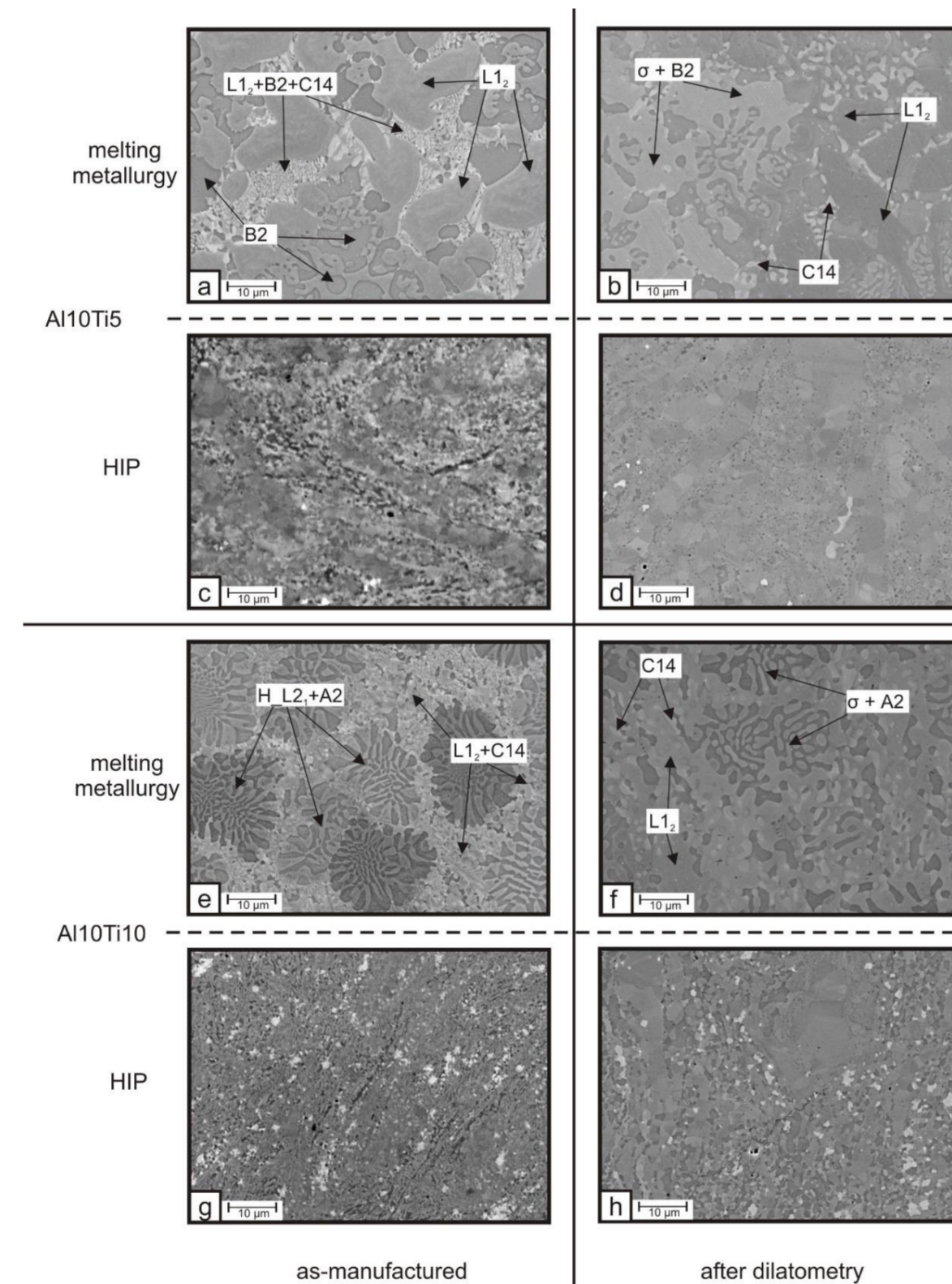


Fig.2 SEM images of compositions Al10Ti5 (a-d) and Al10Ti10 (e-h). Phases are labeled in the images of the samples produced by melting metallurgy.

Quantitative Phase Analysis

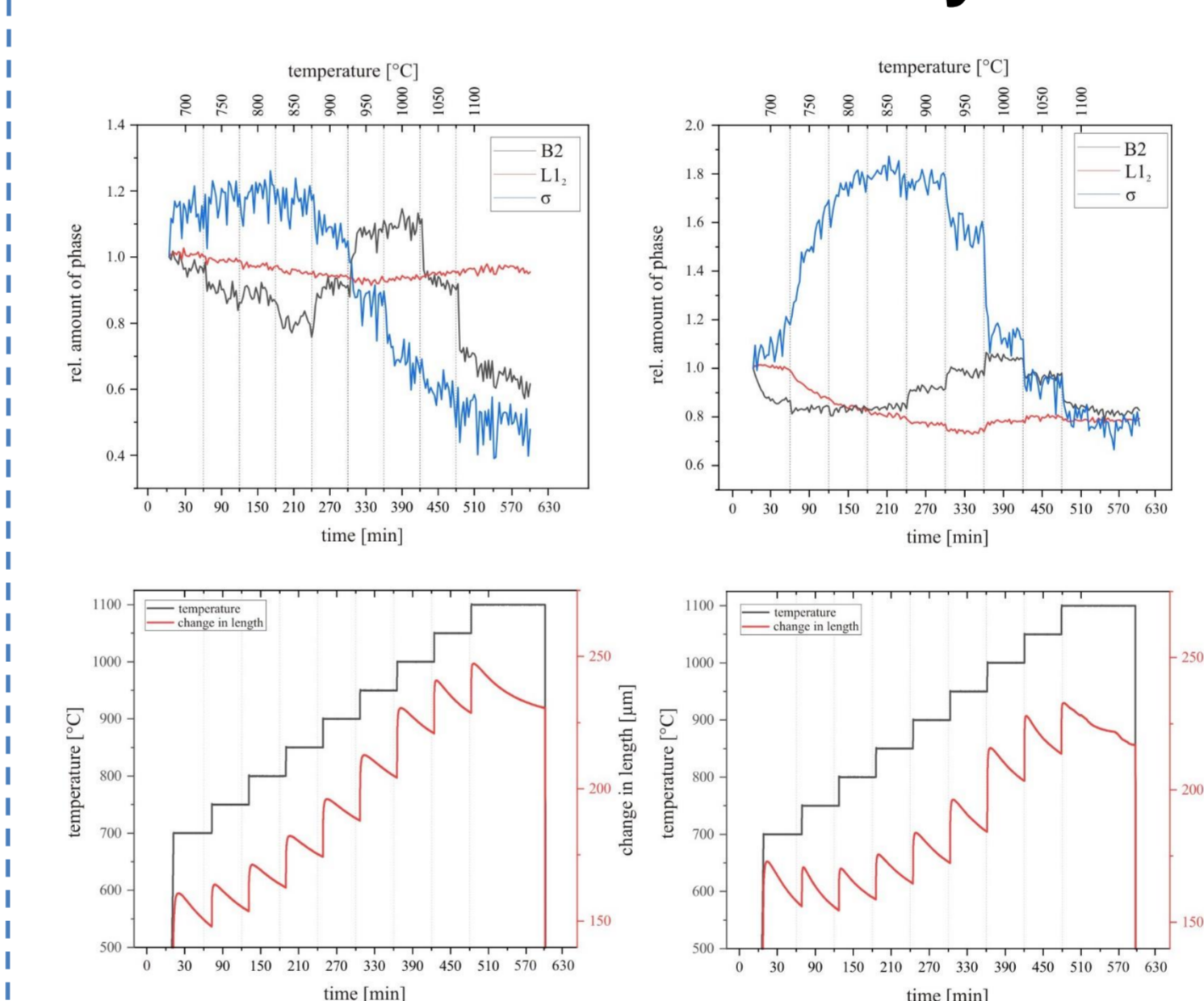


Fig. 3 Overview of the relative amount of phases determined by neutron-diffraction and the change in length and temperature plotted over time. Left: as-HIP Al10Ti5, right: as-HIP Al10Ti10. Since phase fractions differ significantly and the development of the phases are shown in the same diagram, the phase fractions are considered separately and are normalized to their respective values at 700 °C.

M. Reiberg, C. Duan, X. H. Li, E. Werner: High-temperature phase characterization of AlCrFeNiTi compositionally complex alloys; *MATER. CHEM. PHYS.* (2021) 2100163; DOI:10. 1016/j.matchemphys.2021.125272

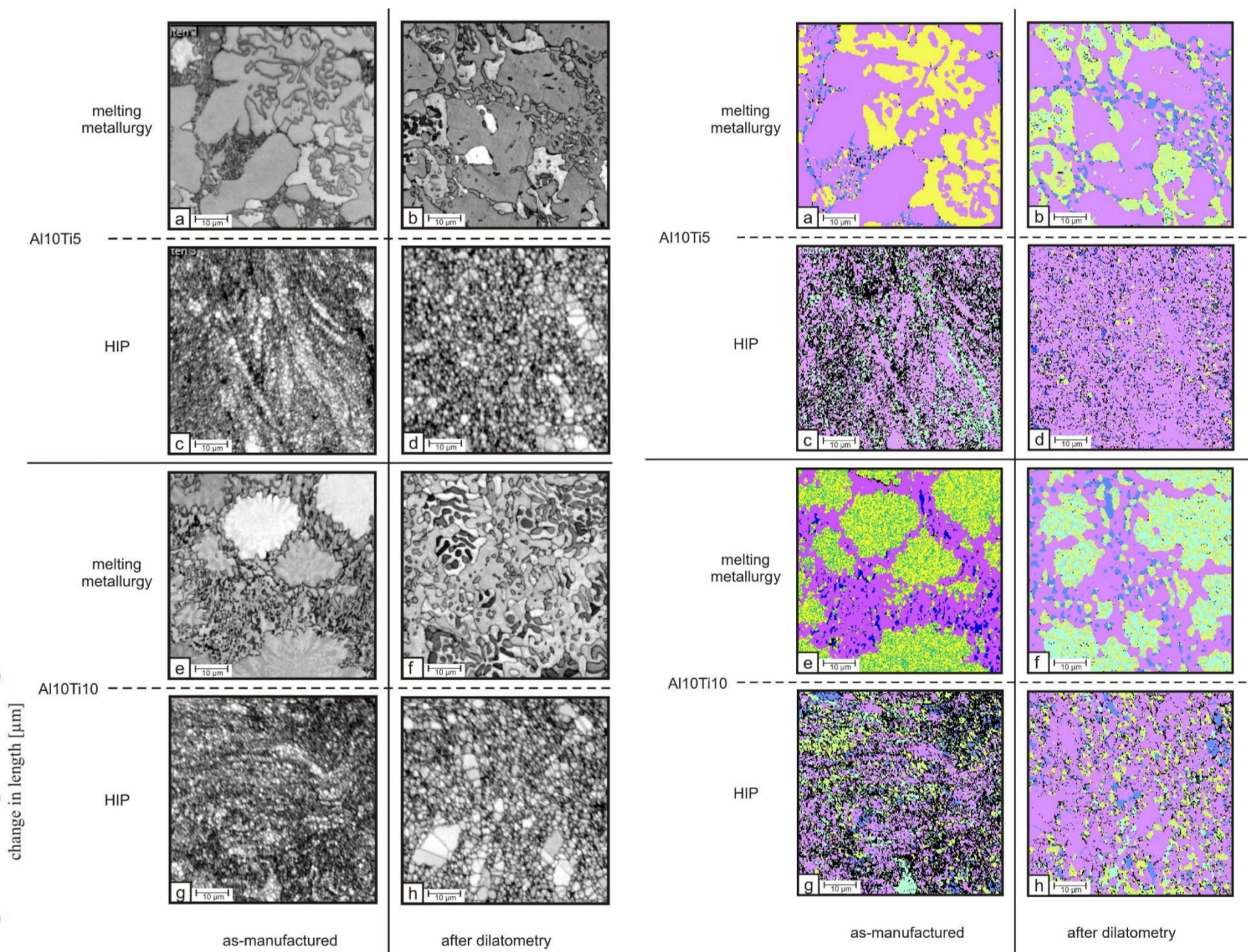


Fig.4 EBSD band contrast images (left) and images with colors of compositions Al10Ti5 (a-d) and Al10Ti10 (e-h). Detected phases are L₁₂ (purple), A₂/B₂ (yellow), σ (turquoise), C₁₄_Laves (blue), Full Heusler (green).

Phase Transition Kinetics in Austempered Ductile Iron (ADI) with Regard to Mo Content

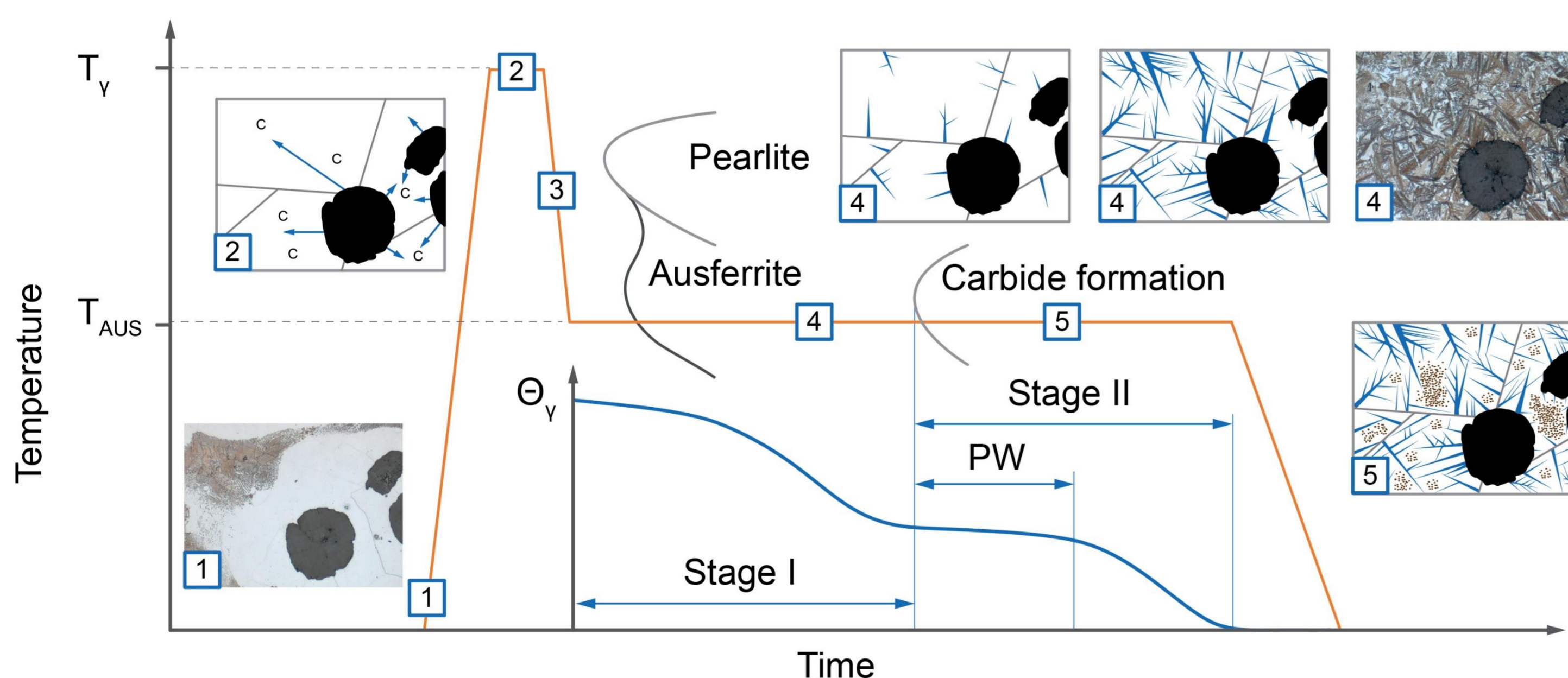


Fig. 5 The course of an ADI heat treatment is exemplarily shown. Starting from the initial state (1) over heating to austenitization temperature T_y (2), followed by quenching (3) to annealing at austempering temperature T_{AUS} and subsequent cooling to room temperature. The evolution of austenite phase fraction φ_A during austempering is schematically depicted. Ausferritic microstructure is formed in the Stage I reaction (4) and followed by the decomposition of retained austenite (5) into carbides and ferrite (Stage II). As long as the loss in austenite fraction is small, the process window (PW) for industrial ADI heat treatments is defined.

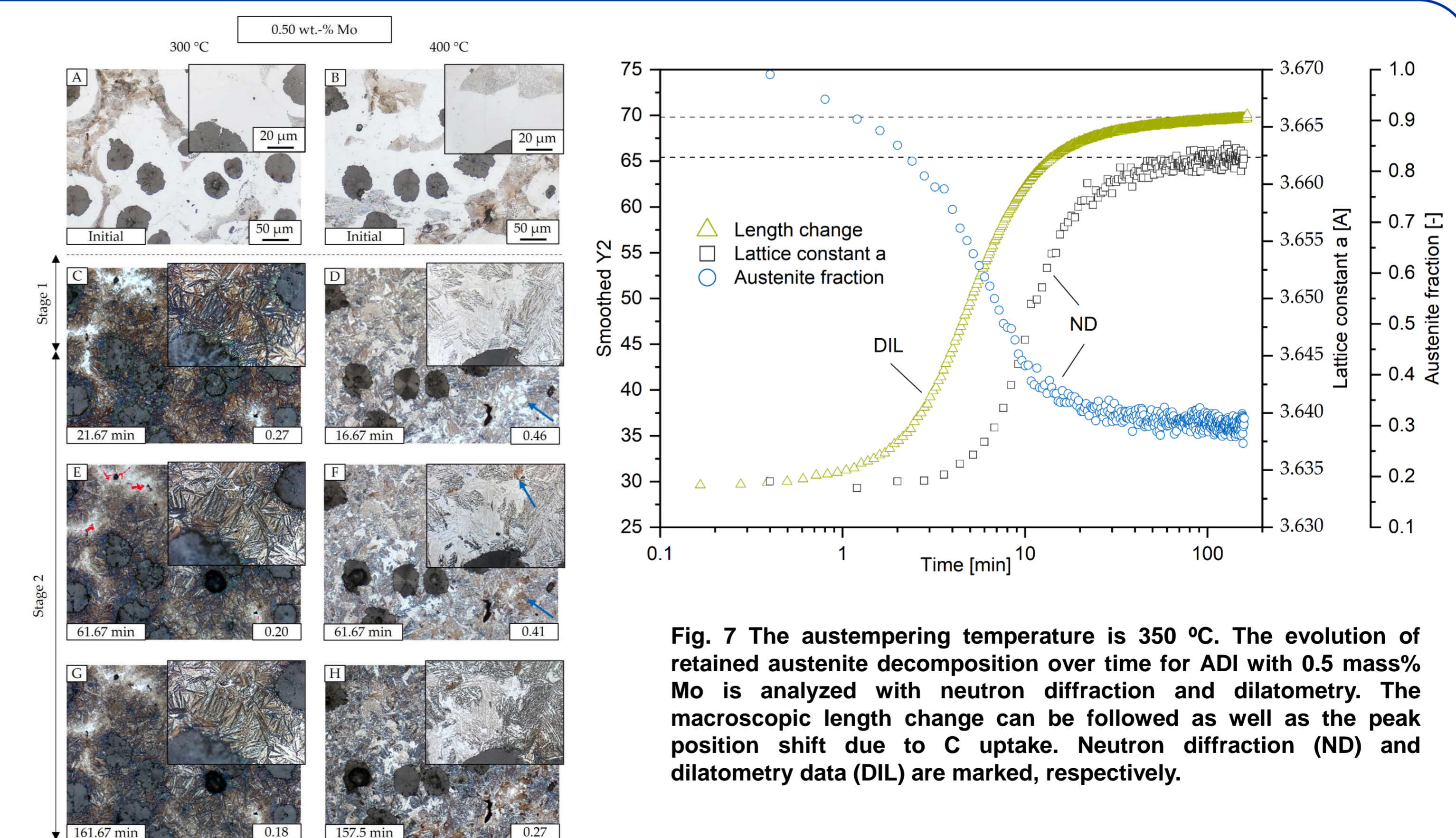


Fig. 6 The evolution of austenite decomposition over time for ADI with 0.5 mass% Mo is shown by Nital etched LOM images. The austempering temperatures are 300 °C (c,e,g) and 400 °C (d,f,h). The initial material state is depicted in (a,b). Carbides in (e) are colored in red.

M. Landesberger, R. Koos, M. Hofmann, X. H. Li, T. Boll, W. Petry and W. Volk: Phase Transition Kinetics in Austempered Ductile Iron (ADI) with Regard to Mo Content; *Materials* (2020), 13, 5266; doi:10.3390/ma13225266